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Article

# A Novel Gold Film-Coated V-Shape Dual-Core Photonic Crystal Fiber Polarization Beam Splitter Covering the E + S + C + L + U Band

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**Abstract:** In this paper, a novel gold film-coated V-shape dual-core photonic crystal fiber (V-DC-PCF) polarization beam splitter (PBS) based on surface plasmon resonance effect is proposed. The coupling lengths of the X-polarization (X-pol) and Y-polarization (Y-pol) and the corresponding coupling length ratio of the proposed V-DC-PCF PBS without gold film and with gold film are compared. The fiber structure parameters and thickness of the gold film are optimized through investigating their effects on the coupling lengths and coupling length ratio. As the propagation length increases, the normalized output powers of the X-pol and Y-pol of the proposed V-DC-PCF PBS at the three wavelengths 1.610, 1.631, and 1.650  $\mu\text{m}$  are demonstrated. The relationships between the extinction ratio (ER), insertion loss (IL) and wavelength for the three splitting lengths (SLs) 188, 185, and 182  $\mu\text{m}$  are investigated. Finally, it is demonstrated that for the proposed V-DC-PCF PBS, the optimal SL is 188  $\mu\text{m}$ , the ILs of the X-pol and Y-pol are less than 0.22 dB, and the splitting bandwidth (SB) can cover the E + S + C + L + U band. The proposed V-DC-PCF PBS has the ultra-short SL, ultra-wide SB, and ultra-low IL, so it is expected to have important applications in the laser, sensing, and dense wavelength division multiplexing systems.

**Keywords:** V-shape dual-core photonic crystal fiber; polarization beam splitter; surface plasmon resonance effect; extinction ratio; insertion loss

## 1. Introduction

Since the first photonic crystal fiber (PCF) was fabricated by Russell et al. in 1996 [1], PCFs have been investigated extensively and applied in different optical fields, such as fiber laser, sensing, optical communication, and so on [2–8]. At present, the PCF-based optical devices, including polarization beam splitter (PBS), polarization filter, modulator, etc., have become the indispensable components in the all-fiber optical systems [9–14].

In recent years, the dual-core PCF (DC-PCF) PBS based on the coupled mode theory has been widely investigated [15–19]. In 2016, Zi et al. reported a simple DC-PCF PBS, whose splitting lengths (SLs) are 249 and 506  $\mu\text{m}$  and splitting bandwidths (SBs) are 17 and 12 nm at wavelengths 1.55 and 1.31  $\mu\text{m}$ , respectively [20]. In the same year, Wang et al. proposed a liquid crystal-filled DC-PCF PBS, whose SL is 890.5  $\mu\text{m}$  and SB covers the



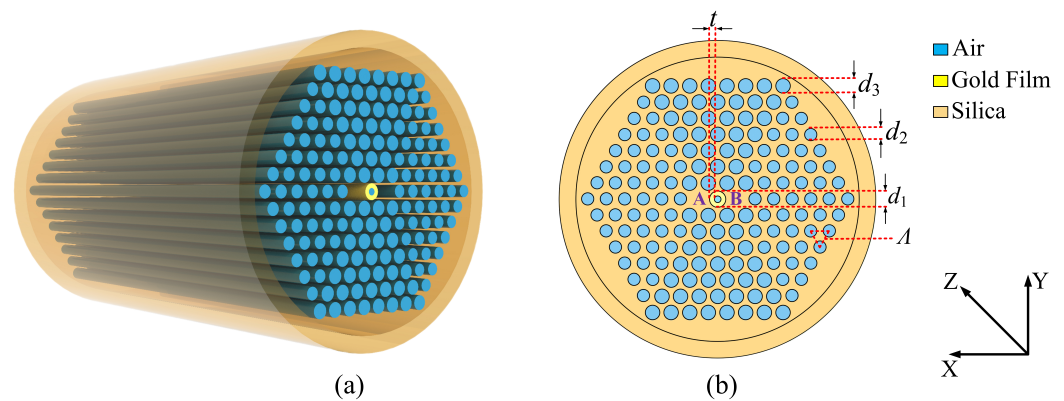
S + C + L band [21]. In 2017, He et al. designed an octagonal lattice DC-PCF PBS with the five elliptical air holes, whose  $SL$  is 105  $\mu\text{m}$  and  $SB$  covers the S + C + L band [22]. In 2017, Wang et al. demonstrated a surface plasmon resonance (SPR) effect-based DC-PCF PBS filled with elliptical gold wire, whose  $SL$  is 1.079 mm and  $SB$  only covers the C band [23]. In 2018, Wang et al. achieved a short DC-PCF PBS with the liquid filled in the central and two elliptical air holes, whose  $SL$  is 78  $\mu\text{m}$  and  $SB$  only covers the C band [24]. In 2019, Lou et al. investigated an ultrashort SPR effect-based DC-PCF PBS coated with gold film, whose  $SL$  is only 47.26  $\mu\text{m}$  and  $SB$  cannot cover the C band [25]. From the previous works, the performances of the DC-PCF PBS can be obviously improved by introducing the elliptical air holes, changing the lattice arrangement of air holes, and selectively filling or coating the air holes with the liquid crystal, liquid, metal wire, and metal film.

Up to now, the fabrication technology of the PCFs with the circular air holes arranged in a hexagonal lattice has been developed more mature [26–32]. Many fabrication methods have been reported, including stack-and-draw, 3D printing, femtosecond laser drilling, etc. [33–39]. In contrast, it is more difficult to fabricate the PCFs when the air holes are arranged in the rectangle and octagonal shapes or the elliptical air holes exist. Especially when selectively filling the metal wire or coating the metal film into the air holes of the PCFs, the difficulty of fabrication is further increased. Since Sazio et al. and Russell et al. Firstly demonstrated the gold film-coated PCF in 2006 [40] and gold wire-filled PCF in 2008 [41], respectively, there are some reports on fabricating the gold film-coated and gold wire-filled PCFs by different methods [42–48]. At present, it is becoming a research hotspot to design and fabricate the gold film-coated or gold wire-filled DC-PCF PBS which has the hexagonal arrangement of circular air holes.

In this paper, we propose a novel gold film-coated V-shape DC-PCF (V-DC-PCF) PBS based on the SPR effect. We compare the coupling lengths ( $CL$ s) of the X-polarization (X-pol) and Y-polarization (Y-pol) and the coupling length ratio ( $CLR$ ) when the proposed V-DC-PCF PBS is coated with and without gold film. At the three wavelengths 1.610, 1.631, and 1.650  $\mu\text{m}$ , the normalized output powers of the X-pol and Y-pol of the V-DC-PCF PBS are demonstrated when the propagation length increases. For the three splitting lengths ( $SL$ s) 188, 185, and 182  $\mu\text{m}$ , the extinction ratio ( $ER$ ) and insertion loss ( $IL$ ) of the proposed V-DC-PCF PBS are investigated. Finally, we obtain a V-DC-PCF PBS with good performances, whose optimal  $SL$ s is 188  $\mu\text{m}$ ,  $IL$ s of the X-pol and Y-pol are less than 0.22 dB, and  $SB$  can cover the E + S + C + L + U band.

## 2. Design of the V-DC-PCF PBS

The three-dimensional and cross-sectional structures of the proposed V-DC-PCF PBS are shown in Figure 1a,b, respectively. From Figure 1a,b, the substrate material is silica, the air holes are arranged in a hexagonal lattice, and the hole to hole pitch is  $\Lambda$ . The most central air hole with the diameter of  $d_1$  is coated with the gold film, which has a thickness of  $t$ . When the light energy is propagated inside the V-DC-PCF coated with gold film, the free electrons on the gold film surface interact with the incident light field, generating the SPR and exciting the surface plasmon polariton (SPP) mode on the gold film surface. At a specific wavelength, the core mode of the V-DC-PCF and SPP mode have the same propagation constant, so the mode coupling occurs due to the phase-matching condition. The two air holes in the first layer along the X-direction of the V-DC-PCF are missing to form the two cores, which are labeled as the cores A and B, respectively. In the cladding region of the V-DC-PCF, there are two other sizes of air holes. The diameter of the smaller air holes on the left and right sides is  $d_2$ , and the diameter of the larger air holes on the upper and lower sides is  $d_3$ . In practice, such a V-DC-PCF can be fabricated with the stack-and-draw method, and the gold film can be selectively coated on the most central air hole by the chemical vapor deposition or magnetron sputtering technique [33,40,47].



**Figure 1.** The three-dimensional (a) and cross-sectional (b) structures of the proposed V-shape dual-core photonic crystal fiber (V-DC-PCF) polarization beam splitter (PBS).

The material dispersion of the silica can be obtained by the Sellmeier equation as [49]

$$n^2(\lambda) = 1 + \frac{A_1\lambda^2}{\lambda^2 - B_1^2} + \frac{A_2\lambda^2}{\lambda^2 - B_2^2} + \frac{A_3\lambda^2}{\lambda^2 - B_3^2} \quad (1)$$

where  $\lambda$  is the wavelength of free space. The related parameters of the Sellmeier equation for the silica material are shown in Table 1.

**Table 1.** The related parameters of the Sellmeier equation for the silica material.

$A_1$	$A_2$	$A_3$	$B_1(\mu\text{m})$	$B_2(\mu\text{m})$	$B_3(\mu\text{m})$
0.6961663	0.4079426	0.8974794	0.0684043	0.1162414	9.896161

The relative dielectric constant of the gold material can be described by the Drude-Lorentz model [50]

$$\varepsilon_m = \varepsilon_\infty - \frac{\omega_D^2}{\omega(\omega - j\gamma_D)} - \frac{\Delta\varepsilon \cdot \Omega_L^2}{(\omega^2 - \Omega_L^2) - j\Gamma_L\omega} \quad (2)$$

where  $\omega$  is the angle frequency of the guided-wave,  $\varepsilon_\infty$  and  $\Delta\varepsilon$  are the high frequency dielectric constant and weighted coefficient,  $\omega_D$  and  $\gamma_D$  are the plasma and damping frequencies, and  $\Omega_L$  and  $\Gamma_L$  are the frequency and bandwidth of the Lorentz oscillator, respectively. The specific parameters of the Drude-Lorentz model for the gold material are shown in Table 2.

**Table 2.** The specific parameters of the Drude-Lorentz model for the gold material.

$\varepsilon_\infty$	$\Delta\varepsilon$	$\omega_D/2\pi(\text{THz})$	$\gamma_D/2\pi(\text{THz})$	$\Omega_L/2\pi(\text{THz})$	$\Gamma_L/2\pi(\text{THz})$
5.9673	1.09	2113.6	15.92	650.07	104.86

The CLs in the X-pol and Y-pol directions of the V-DC-PCF PBS can be described as [51]

$$CL_X = \frac{\lambda}{2|(n_{\text{even}}^X - n_{\text{odd}}^X)|} \quad (3)$$

$$CL_Y = \frac{\lambda}{2|(n_{\text{even}}^Y - n_{\text{odd}}^Y)|} \quad (4)$$

where  $CL_X$  and  $CL_Y$  represent the  $CL$  of the X-pol and Y-pol, respectively,  $\lambda$  is the wavelength of the initial incident light, and  $n_{even}^X$ ,  $n_{odd}^X$ ,  $n_{even}^Y$ , and  $n_{odd}^Y$  represent the effective refractive indices (ERIs) of the even and odd modes in the X-pol and Y-pol, respectively.

The  $CLR$  can be calculated by [52]

$$CLR = \frac{CL_Y}{CL_X} \quad (5)$$

When the  $CLR = 2$  or  $1/2$ , the optimal  $SL$  can be obtained.

For the proposed V-DC-PCF PBS, we only need to consider the case that the initial incident light enters the core A or B since the geometric structure of the cores A and B are identical and symmetrical. In this work, when supposing that the initial incident light entering the core A, the output powers  $P_{out}$  of the X-pol and Y-pol in the core A can be described as [53]

$$P_{out,A}^{X,Y} = P_{in} \cos^2\left(\frac{\pi}{2} \frac{PL}{CL_{X,Y}}\right) \quad (6)$$

where  $P_{in}$  is the power of the initial incident light, and  $PL$  is the propagation length inside the V-DC-PCF PBS.

The  $ER$  of the core A, which is considered as a significant parameter for evaluating the splitting performance of the V-DC-PCF PBS, can be calculated by [54]

$$ER_A = 10 \log_{10} \frac{P_{out,A}^X}{P_{out,A}^Y} \quad (7)$$

The  $IL$  of the X-pol and Y-pol in the core A of the V-DC-PCF PBS can be described as [55]

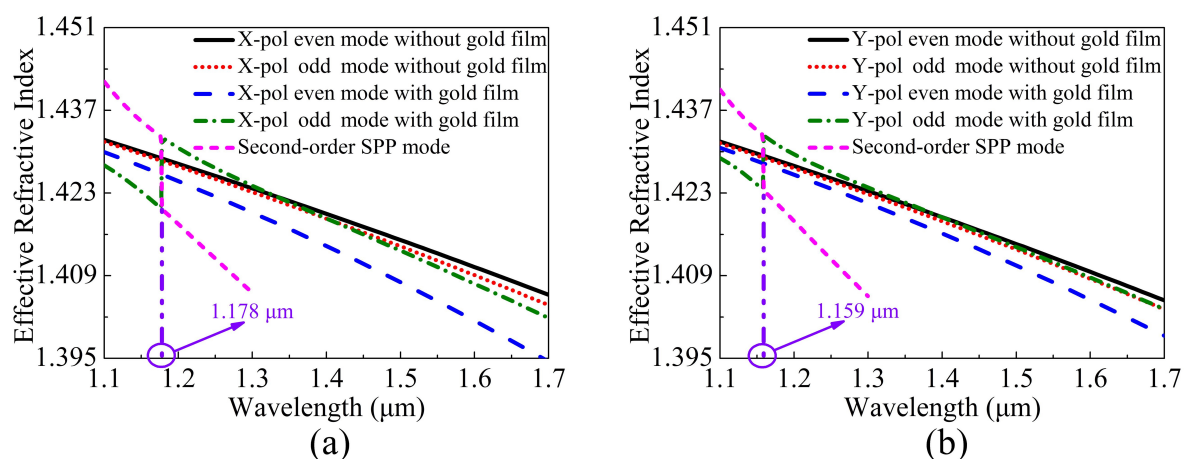
$$IL_{X,Y} = -10 \log_{10} \frac{P_{out,A}^{X,Y}}{P_{in}} \quad (8)$$

### 3. Simulation Results and Discussion

The finite element method is used to investigate the propagation characteristics of the proposed V-DC-PCF [56,57]. The initial fiber structure parameters are set as following:  $d_1 = 0.95 \mu\text{m}$ ,  $d_2 = 1.20 \mu\text{m}$ ,  $d_3 = 1.40 \mu\text{m}$ ,  $\Lambda = 2.20 \mu\text{m}$ , and  $t = 55 \text{ nm}$ . In the simulation, the material coefficients including the refractive indices of the silica and air and the relative dielectric constant of the gold material are set after the simulation model is established. Then, a perfect matching layer (PML), whose thickness is  $10 \mu\text{m}$  and refractive index is  $n_{\text{silica}} + 0.03$ , is added to the outermost edge of the gold film-coated V-DC-PCF so as to absorb the radiation energy [58]. Moreover, the grid sizes of the silica, air holes, and PML are set as  $\lambda/4$ , and the grid size of the most central air hole coated with gold film is set as  $\lambda/6$ .

When the V-DC-PCF is coated without gold film and with gold film, the ERIs of the X-pol and Y-pol even and odd modes and second-order SPP mode are shown in Figure 2a,b, respectively. It can be seen from Figure 2a,b that for the V-DC-PCF without gold film, the ERIs of the X-pol and Y-pol even and odd modes decrease approximately linearly with the increase of wavelength. Moreover, the ERIs of the X-pol and Y-pol odd modes decrease more obviously than that of the X-pol and Y-pol even modes at the longer wavelength side, but the differences between the X-pol or Y-pol even and odd modes are very small. According to Equations (3) and (4), we can infer that the  $CL_X$  and  $CL_Y$  will also change in the approximately linear trend and have large values. In contrast, when the V-DC-PCF is coated with gold film, the ERIs of the X-pol and Y-pol even modes still decrease approximately linearly as the wavelength increases. However, there are two cross points between the ERIs of the X-pol and Y-pol odd modes and second-order SPP mode at wavelengths  $1.178$  and  $1.159 \mu\text{m}$ , respectively, where the phase-matching condition is satisfied. According to the coupled mode theory, the X-pol and Y-pol odd modes occur to

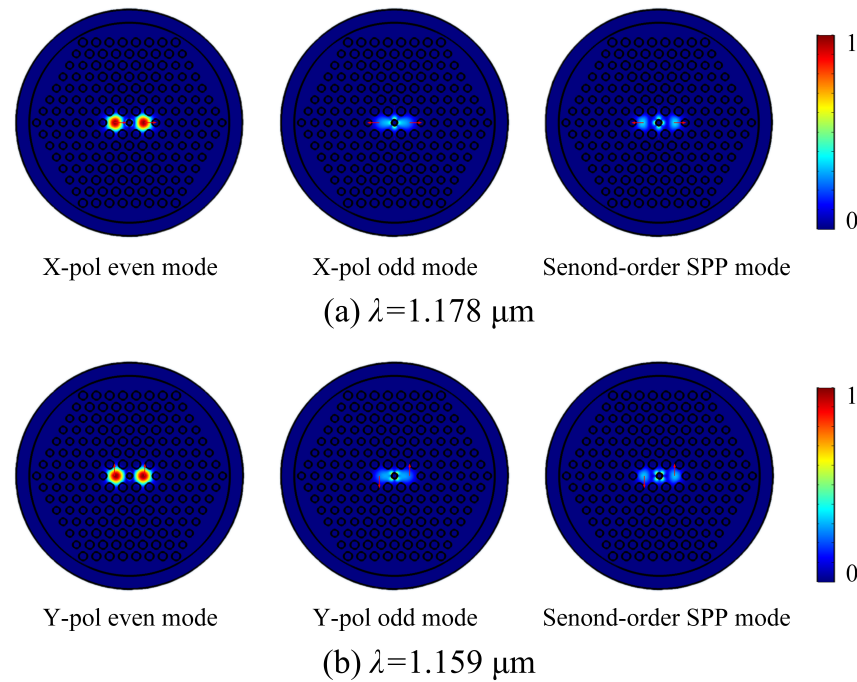
couple with the second-order SPP mode at wavelengths 1.178 and 1.159  $\mu\text{m}$ , respectively. In addition, it can be seen from Figure 2a,b that before the phase-matching wavelengths, the ERIs of the X-pol and Y-pol odd modes decrease rapidly, along with a relatively small and stable slope. Hence, the differences between the ERIs of the X-pol and Y-pol even and odd modes increase rapidly with the increase of wavelength. The ERIs of the X-pol and Y-pol odd modes increase significantly at wavelengths 1.178 and 1.159  $\mu\text{m}$ , respectively, and there are maximum differences between the ERIs of the X-pol and Y-pol even and odd modes. Thus, the  $CL_X$  and  $CL_Y$  will have significant changes at wavelengths 1.178 and 1.159  $\mu\text{m}$ , respectively. But after the phase-matching wavelengths, the ERIs of the X-pol and Y-pol odd modes first decrease rapidly and then maintain a relatively stable slope. Finally, the relatively stable slope of the ERIs of the X-pol and Y-pol odd modes will be smaller than that of the ERIs of the X-pol and Y-pol even modes as the wavelength increases. Therefore, the differences between the ERIs of the X-pol and Y-pol even and odd modes first decrease and then increase as the wavelength increases. Figure 3a,b show the mode field distributions of the X-pol and Y-pol even and odd modes and second-order SPP mode calculated at wavelengths 1.178 and 1.159  $\mu\text{m}$ , respectively. From Figure 3a,b, the mode field distributions of the X-pol and Y-pol even modes have no change at wavelengths 1.178 and 1.159  $\mu\text{m}$ , respectively. But the mode field energies of the X-pol and Y-pol odd modes and second-order SPP mode occur to transfer at the two wavelengths. It further confirms the previous conclusion that only the X-pol and Y-pol odd modes and second-order SPP mode occur to couple at the phase-matching wavelengths.



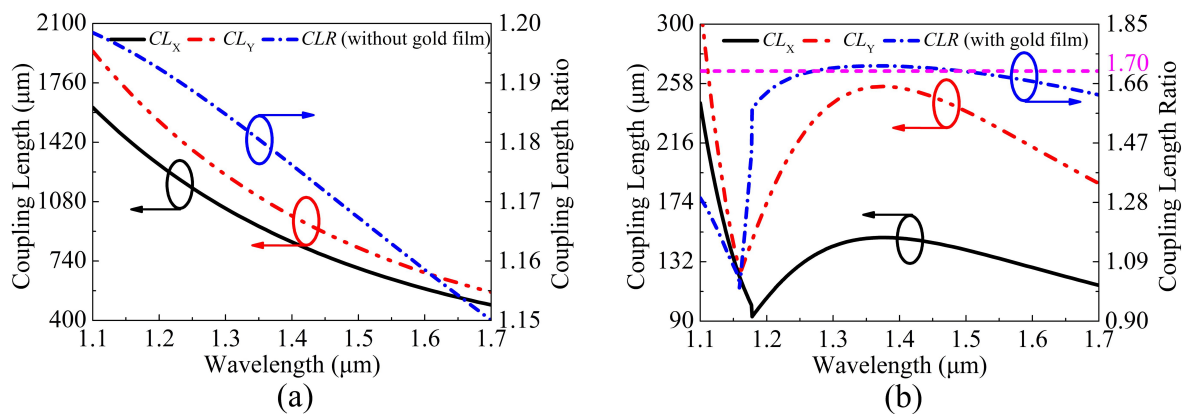
**Figure 2.** The ERIs of the (a) X-pol and (b) Y-pol even and odd modes and second-order surface plasmon polariton (SPP) mode calculated as functions of wavelength when the V-DC-PCF is coated without gold film and with gold film, respectively.

The relationships between the  $CL_X$ ,  $CL_Y$ , and  $CLR$  and wavelength are shown in Figure 4a,b, respectively, when the V-DC-PCF is coated without gold film and with gold film. It can be seen from Figure 4a that when the V-DC-PCF is coated without gold film, the  $CL_X$  and  $CL_Y$  decrease gradually, and the corresponding  $CLR$  also decreases in an approximately linear trend as the wavelength increases. According to Equations (3) and (4) and the above analysis, when the V-DC-PCF is coated with gold film, the  $CL_X$  and  $CL_Y$  decrease rapidly before the phase-matching wavelengths, and occur to change significantly at wavelengths 1.178 and 1.159  $\mu\text{m}$ , respectively, as shown in Figure 4b. After the phase-matching wavelengths, the  $CL_X$  and  $CL_Y$  increase first and then decrease. At this time, according to Equation (5), the  $CLR$  decreases rapidly before wavelength 1.159  $\mu\text{m}$ , has a significant change between wavelength 1.159 and 1.178  $\mu\text{m}$ , and increases first and then decreases after wavelength 1.178  $\mu\text{m}$ . However, after wavelength 1.178  $\mu\text{m}$ , the overall change of the  $CLR$  is relatively flat. In addition, the  $CLR$  has the two intersections, where the  $CLR$  is equal to 1.7. By comparing Figure 4a,b, the maximum  $CL$  for the V-DC-PCF with gold film is smaller than the minimum  $CL$  for the V-DC-PCF without gold film, which

has a direct effect on the  $SL$  of the V-DC-PCF PBS. From the above analysis, it is possible to achieve a PBS with the shorter  $SL$  and larger  $SB$  by using a V-DC-PCF with gold film.



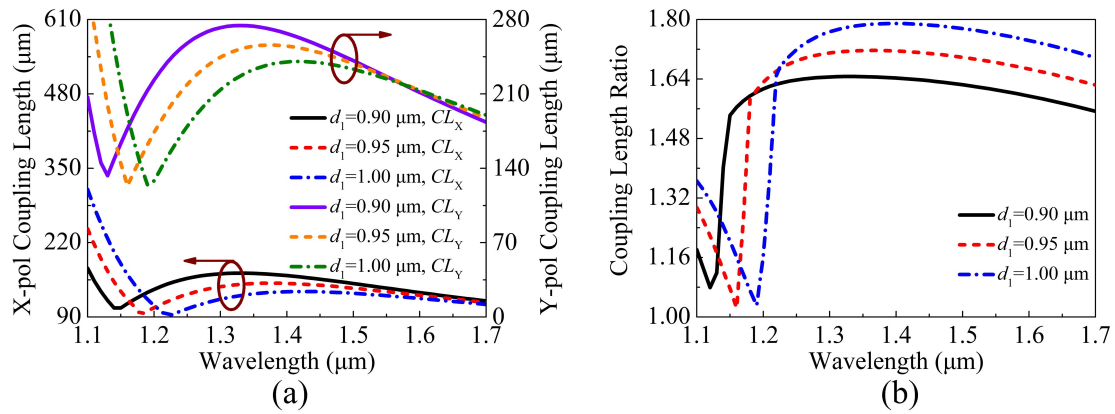
**Figure 3.** The mode field distributions of the (a) X-pol and (b) Y-pol even and odd modes and second-order SPP mode of the V-DC-PCF calculated at wavelengths 1.178 and 1.159  $\mu\text{m}$ , respectively.



**Figure 4.** The  $CL_X$ ,  $CL_Y$ , and  $CLR$  as functions of the wavelength when the V-DC-PCF is coated (a) without gold film and (b) with gold film.

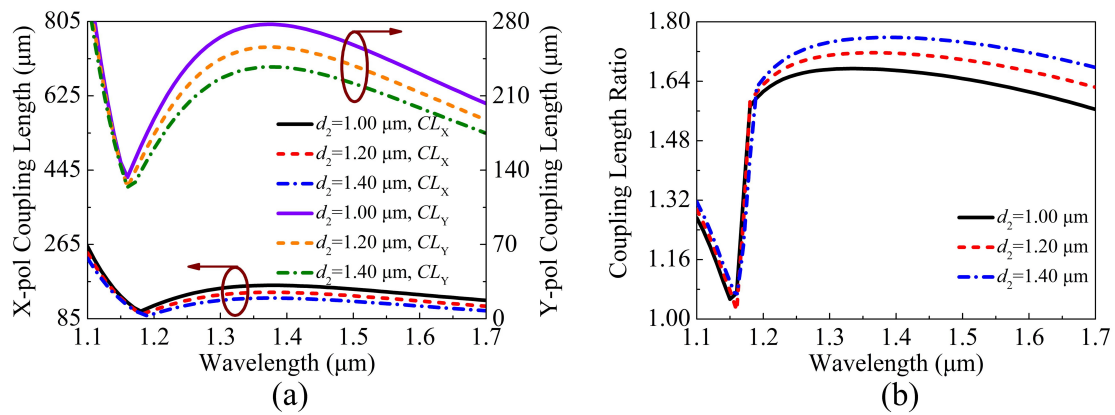
The structure parameters of the proposed V-DC-PCF PBS with gold film need to be optimized to satisfy the condition of  $CLR = 2$ , which corresponds to the optimal  $SL$ . When the fiber structure parameters, including  $d_1$ ,  $d_2$ ,  $d_3$ ,  $\Lambda$ , and  $t$  are changed, respectively, the ERIs of the X-pol and Y-pol even and odd modes will occur to change in different degrees, which can also cause the changes of the  $CL_X$ ,  $CL_Y$ , and  $CLR$ . The variations of the  $CL_X$ ,  $CL_Y$ , and  $CLR$  of the proposed V-DC-PCF PBS are shown in Figure 5a,b when  $d_1$  is chosen as 0.90, 0.95, and 1.00  $\mu\text{m}$ , respectively. It can be seen from Figure 5a that the  $CL_X$  and  $CL_Y$  decrease as  $d_1$  increases at the short wavelength side. At the long wavelength side, as  $d_1$  increases, the  $CL_X$  still decreases slightly, while the  $CL_Y$  shows a slightly increased trend. The  $CLR$  gradually increases as  $d_1$  increases, and the phase-matching wavelength occurs to red-shift, as shown in Figure 5b.





**Figure 5.** The variations of the (a)  $CL_X$ ,  $CL_Y$ , and (b)  $CLR$  of the proposed V-DC-PCF PBS for different  $d_1$ .

The variations of the  $CL_X$ ,  $CL_Y$ , and  $CLR$  of the proposed V-DC-PCF PBS are shown in Figure 6a,b when  $d_2$  is chosen as 1.00, 1.20, and 1.40 μm, respectively. It can be seen from Figure 6a,b that as  $d_2$  increases, the  $CL_X$  and  $CL_Y$  gradually decrease while the  $CLR$  shows an increased trend. In addition, the change of the phase-matching wavelength is not obvious, and only a slight red-shift occurs as  $d_2$  increases.

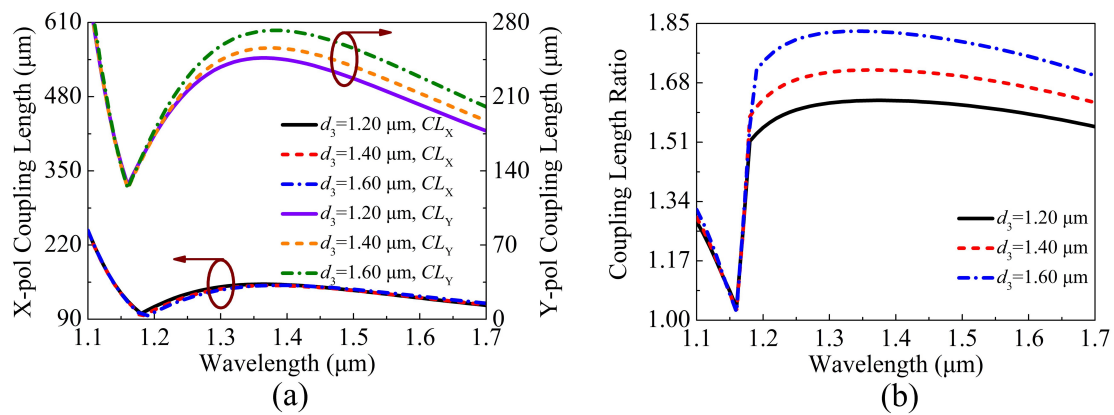


**Figure 6.** The variations of the (a)  $CL_X$ ,  $CL_Y$ , and (b)  $CLR$  of the proposed V-DC-PCF PBS for different  $d_2$ .

When  $d_3$  is chosen as 1.20, 1.40, and 1.60 μm, respectively, the variations of the  $CL_X$ ,  $CL_Y$ , and  $CLR$  of the proposed V-DC-PCF PBS are shown in Figure 7a,b. From Figure 7a, as  $d_3$  increases, the  $CL_X$  decreases slightly at the short wavelength side and remains nearly unchanged at the long wavelength side. In comparison, the  $CL_Y$  gradually increases as  $d_3$  increases, and the corresponding change amplitude at the long wavelength side is larger than that at the short wavelength side. As shown in Figure 7b, as  $d_3$  increases, the  $CLR$  gradually increases, and the position of the phase-matching wavelength remains unchanged.

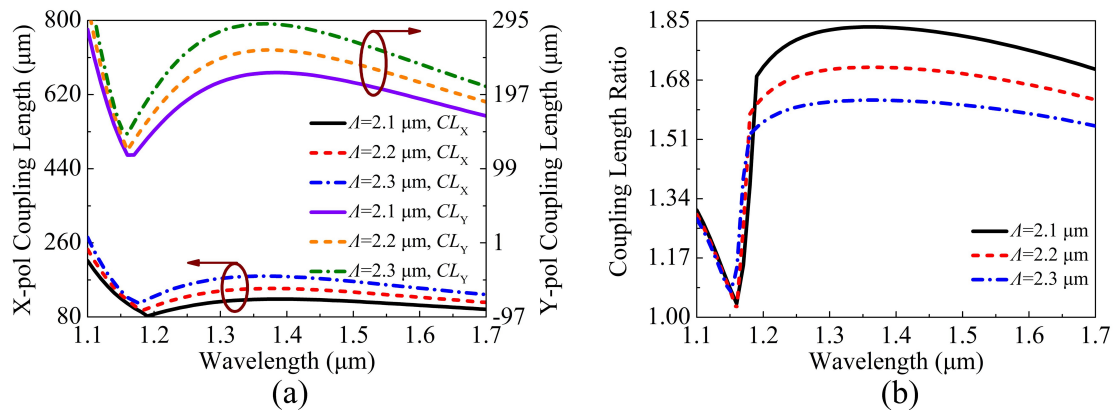
The variations of the  $CL_X$ ,  $CL_Y$  and  $CLR$  of the proposed V-DC-PCF PBS are shown in Figure 8a,b when  $\Lambda$  is chosen as 2.1, 2.2, and 2.3 μm, respectively. Figure 8a,b, as  $\Lambda$  increases, the  $CL_X$  and  $CL_Y$  gradually increase, but the  $CLR$  shows a decreasing trend. In addition, the change of the phase-matching wavelength is not obvious, along with a small shift towards the short wavelength side. By comparing the results shown in Figures 5b, 6b, 7b, and 8b, it is found that the change of  $\Lambda$  has the most remarkable influence on the  $CLR$ .



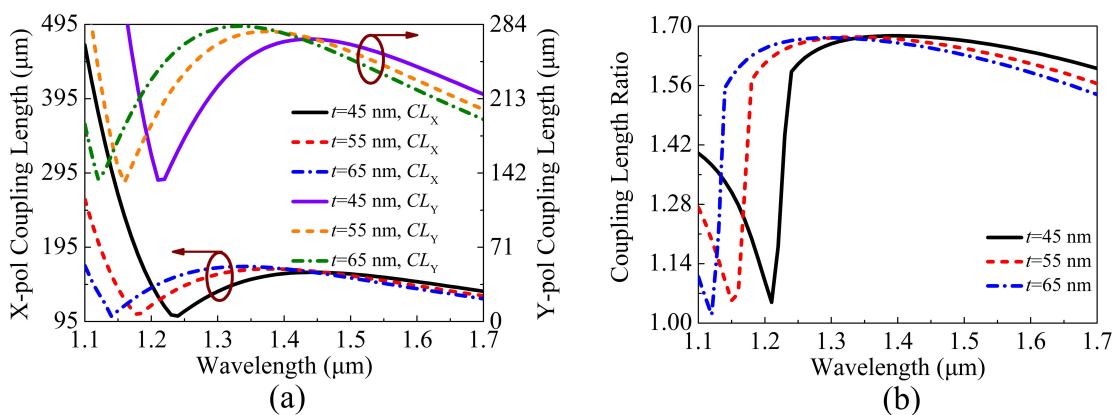


**Figure 7.** The variations of the (a)  $CL_X$ ,  $CL_Y$ , and (b)  $CLR$  of the proposed V-DC-PCF PBS for different  $d_3$ .

Figure 9a,b show the variations of the  $CL_X$ ,  $CL_Y$ , and  $CLR$  of the proposed V-DC-PCF PBS when  $t$  is chosen as 45, 55, and 65 nm, respectively. It can be seen from Figure 9a that as  $t$  increases, the  $CL_X$  and  $CL_Y$  increase at the short wavelength side and decrease at the long wavelength side. It can be seen from Figure 9b that as  $t$  increases, the  $CLR$  increases at the short wavelength side and decreases at the long wavelength side, and the position of the phase-matching wavelength gradually shifts towards the short wavelength side.



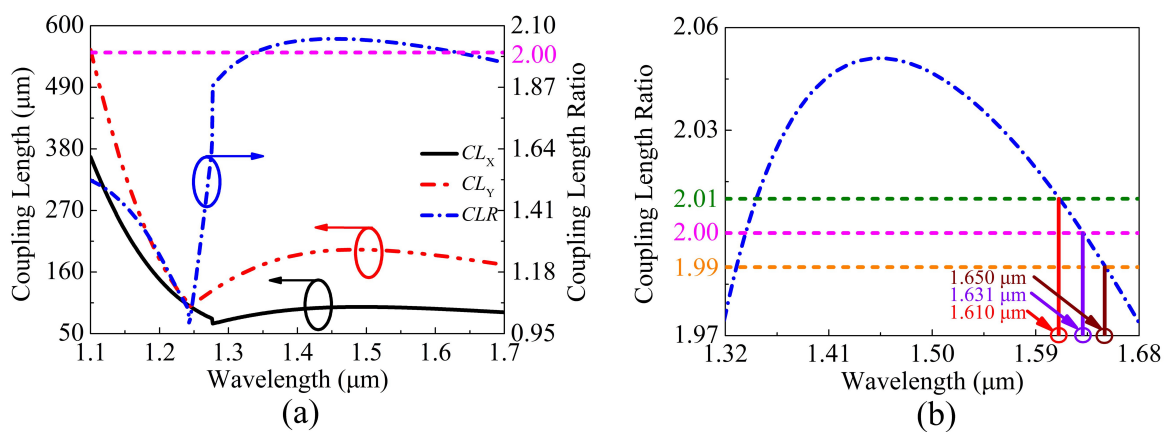
**Figure 8.** The variations of the (a)  $CL_X$ ,  $CL_Y$ , and (b)  $CLR$  of the proposed V-DC-PCF PBS for different  $\Lambda$ .



**Figure 9.** The variations of the (a)  $CL_X$ ,  $CL_Y$ , and (b)  $CLR$  of the proposed V-DC-PCF PBS for different  $t$ .

Based on the above analysis, the influence rule of the structure parameters of the proposed V-DC-PCF PBS on the  $CL_X$ ,  $CL_Y$ , and  $CLR$  can be clearly known. Thus, the empirical steps for designing such a V-DC-PCF PBS can be summarized as following. First,

by together adjusting  $d_1$  and  $t$ , the phase-matching condition can be achieved at the shorter wavelength, and the value of the  $CLR$  is close to 2. At this time, a relatively flat  $CLR$  curve can be obtained in the desired band. Second, by together adjusting  $d_2$ ,  $d_3$ , and  $\Lambda$ , the  $CLR$  curve with the relatively flat profile and the value of 2 can be obtained when the phase-matching wavelength does not change obviously. Thus, the optimized structure parameters of the proposed V-DC-PCF PBS are chosen as follows:  $d_1 = 1.00 \mu\text{m}$ ,  $d_2 = 1.41 \mu\text{m}$ ,  $d_3 = 1.50 \mu\text{m}$ ,  $\Lambda = 2.10 \mu\text{m}$ , and  $t = 46.5 \text{ nm}$ . At this time, the variations of the optimal  $CL_X$ ,  $CL_Y$ , and  $CLR$  of the proposed V-DC-PCF PBS and the corresponding zoomed flat region of the  $CLR$  are shown in Figure 10a,b, respectively. From Figure 10a, the  $CL_X$  and  $CL_Y$  have significant changes at the phase-matching wavelengths 1.277 and 1.243  $\mu\text{m}$ , respectively. Moreover, the  $CLR$  is approximately equal to 2 in a wide wavelength range of above 1.277  $\mu\text{m}$ . From Figure 10b, the value of the  $CLR$  changes from 1.974 to 2.051 in the wavelength range from 1.32 to 1.68  $\mu\text{m}$ , and the maximum difference of the  $CLR$  between wavelength 1.32 and 1.68  $\mu\text{m}$  is 0.077. In addition, the values of the  $CLR$  at wavelengths 1.610, 1.631, and 1.650  $\mu\text{m}$  are 2.01, 2.00, and 1.99, respectively, which are approximately equal to 2. It is worth noting that although the value of the  $CLR$  is also equal to 1.99, 2.00, and 2.01 at other three shorter wavelengths, but the corresponding slope variation of the  $CLR$  is larger, which will affect the overall bandwidth to a great extent.



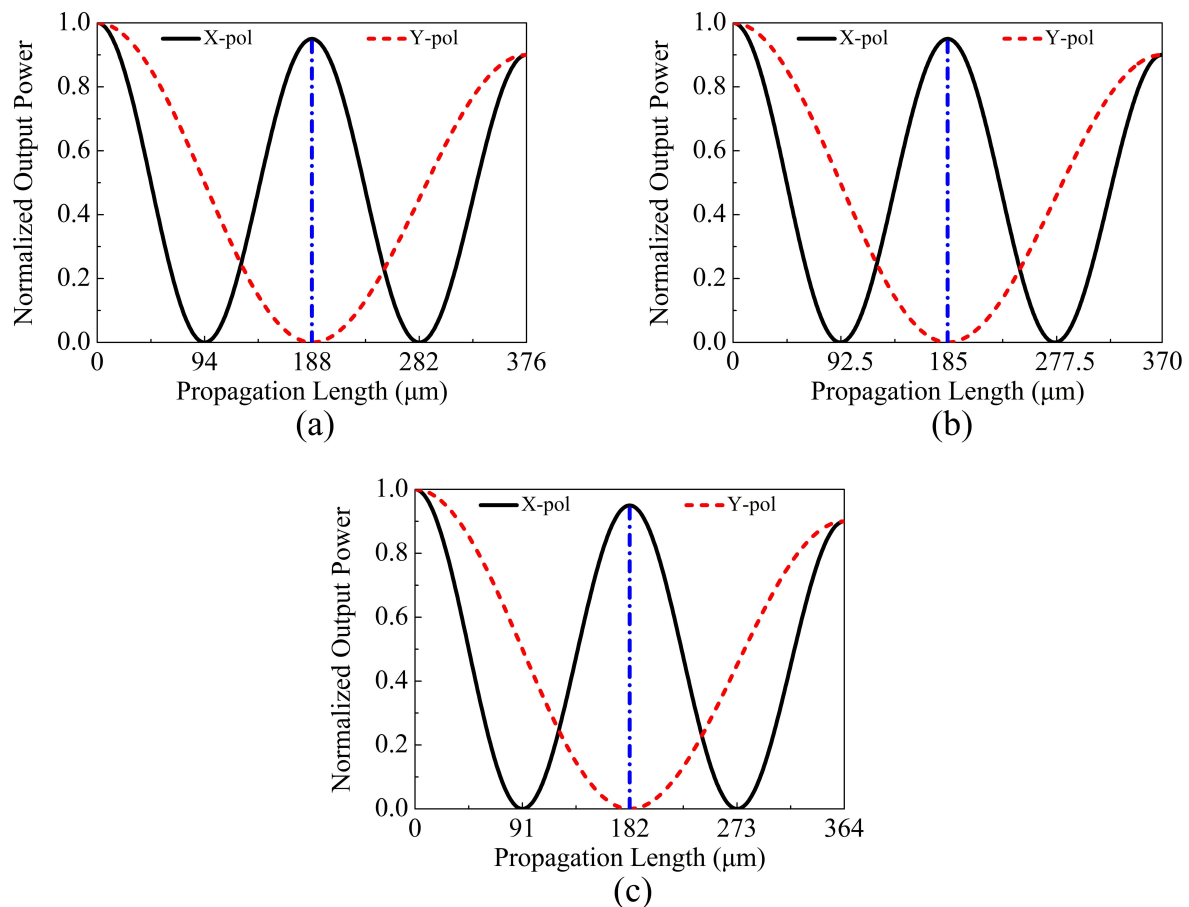
**Figure 10.** The optimal  $CL_X$ ,  $CL_Y$ , and  $CLR$  of the proposed V-DC-PCF PBS, and (b) the zoomed flat region of the  $CLR$ .

In the following, the relationships between the output powers  $P_{out}$  of the X-pol and Y-pol of the proposed V-DC-PCF PBS and  $PL$  at the three wavelengths 1.610, 1.631, and 1.650  $\mu\text{m}$  are shown in Figure 11a–c, respectively. From Figure 11a–c,  $P_{out}$  of the X-pol reaches the maximum values when the  $PL$  is located at 188, 185, and 182  $\mu\text{m}$ , respectively. In contrast, the corresponding  $P_{out}$  of the Y-pol reaches 0 when the  $PL$  is located at 188, 185, and 182  $\mu\text{m}$ , respectively. This phenomenon indicates that the X-pol light only exists in the core A while the Y-pol light only exists in the core B at the three  $PL$ s. Therefore, the  $SL$  of the proposed V-DC-PCF PBS may be 182, 185, or 188  $\mu\text{m}$ . Moreover, another notable phenomenon is that the total  $P_{out}$  decreases slightly as the  $PL$  increases. This is mainly because a fraction of the energy always propagates on the surface of the gold film, leading to the increase of the ohmic loss.

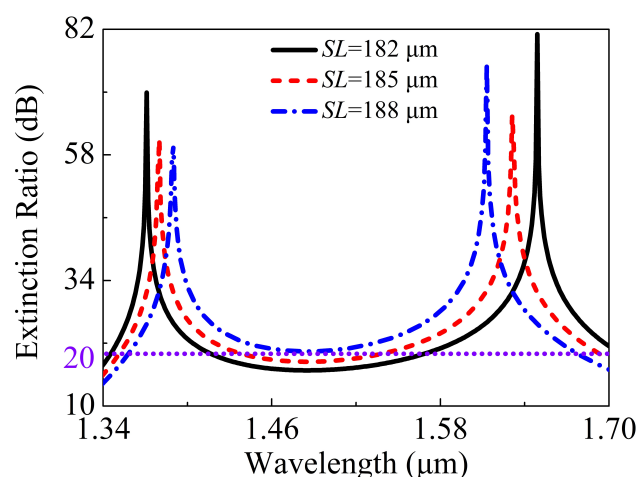
When the  $SL$  is equal to 182, 185, and 188  $\mu\text{m}$ , respectively, the relationships between the  $ER$ s in the core A of the proposed V-DC-PCF PBS and wavelength are shown in Figure 12. It can be seen from Figure 12 that for the  $SL$ s of 182 and 185  $\mu\text{m}$ , the  $ER$ s are less than 20 dB in some wavelength ranges. In contrast, when  $SL$  is equal to 188  $\mu\text{m}$ , the  $ER$  is always larger than 20 dB in a wide wavelength range from 1.359 to 1.677  $\mu\text{m}$ . Figure 13 shows the relationships between the  $IL$ s of the X-pol and Y-pol in the core A of the proposed V-DC-PCF PBS and wavelength when the  $SL$  is equal to 182, 185, and 188  $\mu\text{m}$ , respectively. From Figure 13, for the  $SL$ s of 182, 185, and 188  $\mu\text{m}$ , the maximum  $IL$  of the X-pol and Y-pol is 0.22 dB in the wavelength range of 1.359 to 1.677  $\mu\text{m}$ . Such a small

$IL$  can meet the actual application requirements. Because the proposed V-DC-PCF PBS has the ultra-short  $SL$ , the bending loss can be neglected. Therefore, we can draw a conclusion that for the proposed V-DC-PCF PBS, the optimal  $SL$  is  $188\ \mu\text{m}$ , the  $SB$  covers the entire E + S + C + L + U band, and the  $IL$ s of the X-pol and Y-pol are less than 0.22 dB.

The comparisons between the proposed V-DC-PCF PBS and reported SPR-based DC-PCF PBS are shown in Table 3. From Table 3, only the  $SB$  of the SPR-based DC-PCF PBS reported in Ref [12] is larger than that of the proposed V-DC-PCF PBS. However, in Ref [12], the  $SL$  and minimum  $IL$  are  $4.036\ \text{mm}$  and  $0.8\ \text{dB}$ , respectively, while they are only  $188\ \mu\text{m}$  and  $0.22\ \text{dB}$  in this work. Moreover, the air holes of the DC-PCF PBS reported in Ref [12] are arranged in a square lattice, so it is difficult to fabricate. In addition, only the  $SL$  of the SPR-based DC-PCF PBS reported in Ref [25] is shorter than that of this work. However, in Ref [25], the  $SB$ , which covers the S + C + L band, is much narrower than that of this work, and the  $IL$  is not given. Moreover, the air holes of square lattice of the DC-PCF PBS reported in Ref [25] also increase the difficulty of fabrication. In summary, the proposed V-DC-PCF PBS has the good comprehensive performances.



**Figure 11.** The relationships between the output powers  $P_{out}$  of the X and Y-pol of the proposed V-DC-PCF PBS and  $PL$  at the three wavelengths (a) 1.610, (b) 1.631, and (c) 1.650  $\mu\text{m}$ , respectively.

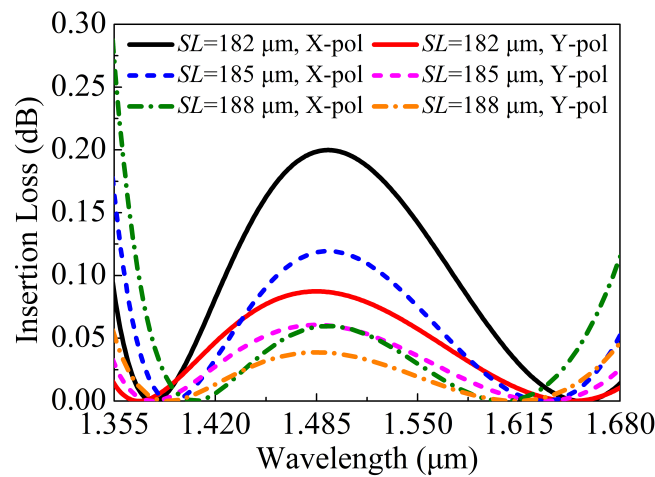


**Figure 12.** The ERs in the core A of the proposed V-DC-PCF PBS as functions of the wavelength for different  $SL$ .

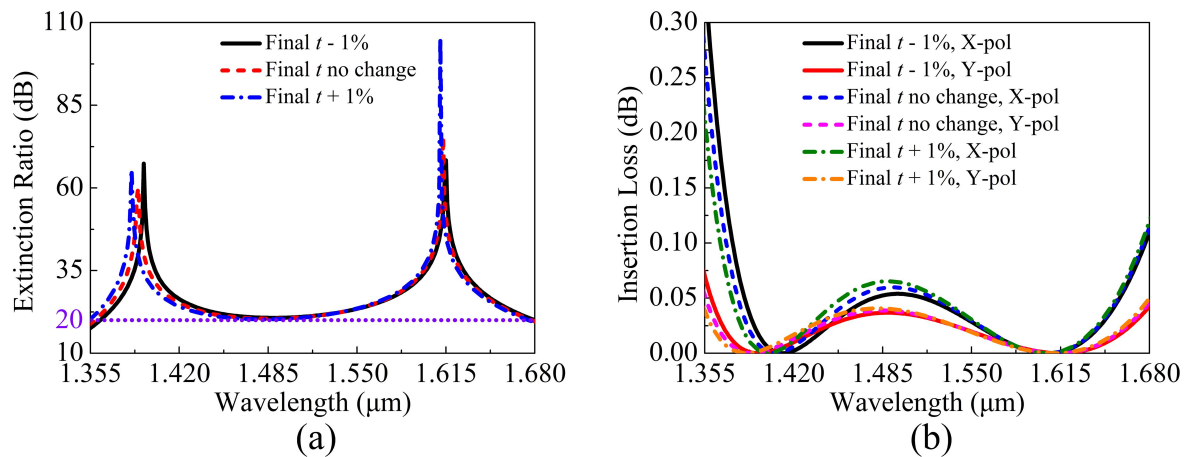
**Table 3.** Comparisons between the proposed V-DC-PCF PBS and reported surface plasmon resonance (SPR)-based DC-PCF PBS.

Ref.	DC-PCF Structure	Gold Film or Wire	SB	SL	Max IL
[12]	Square lattice with circular air holes	Gold wire	O + E + S + C + L + U band	4.036 mm	0.8 dB
[13]	Hexagonal lattice with elliptical air holes	Gold wire	S + C + L + U band	254.6 $\mu\text{m}$	N/A
[14]	Hexagonal lattice with circular air holes	Gold wire	O and C bands	830 $\mu\text{m}$	N/A
[15]	D-shape hexagonal lattice with circular air holes	Gold film	C band	0.782 mm	1.5 dB
[16]	Hexagonal lattice with circular air holes	Gold wire	S + C + L + U band	577.5 $\mu\text{m}$	N/A
[17]	Rectangle lattice with circular air holes	Two gold wires	E + C band	1 mm	N/A
[18]	Hexagonal lattice with circular air holes	Gold film	S + C + L band	5.112 mm	N/A
[24]	Hexagonal lattice with circular air holes	Elliptical gold wire	C band	1.079 mm	N/A
[25]	Square lattice with circular air holes	Gold film	S + C + L band	47.26 $\mu\text{m}$	N/A
This work	Hexagonal lattice with circular air holes	Gold film	E + S + C + L + U band	188 $\mu\text{m}$	<0.22 dB

The ERs in the core A and ILs of the X-pol and Y-pol in the core A of the proposed V-DC-PCF PBS are shown in Figure 14a,b when  $t$  changes  $\pm 1\%$ . From Figure 14a, the wavelength range of the ER larger than 20 dB changes slightly, which indicates that the proposed V-DC-PCF PBS still has a wide SB. From Figure 14b, the ILs of the X-pol and Y-pol are always less than 0.22 dB in each SB. Thus,  $t$  has good error-tolerant rate in the actual coating process.



**Figure 13.** The  $IL$ s of the X-pol and Y-pol in the core A of the proposed V-DC-PCF PBS as functions of the wavelength for different  $SL$ .



**Figure 14.** (a)  $ER$ s in the core A and (b)  $IL$ s of the X-pol and Y-pol in the core A of the proposed V-DC-PCF PBS as functions of wavelength when  $t$  has the distortion of  $\pm 1\%$ .

#### 4. Conclusions

In summary, a novel gold film-coated V-DC-PCF PBS based on the SPR effect is proposed. The  $CL_X$ ,  $CL_Y$ , and  $CLR$  of the proposed V-DC-PCF PBS coated without gold film and with gold film are investigated. The empirical steps for designing such a V-DC-PCF PBS are summarized by analyzing the effects of the fiber structure parameters on the  $CL_X$ ,  $CL_Y$ , and  $CLR$ . The  $CLR$  of 2 can be obtained at the three wavelengths 1.610, 1.631, and 1.650  $\mu\text{m}$ . When the  $SL$ s are equal to 188, 185, and 182  $\mu\text{m}$ , the relationships between the  $ER$ ,  $IL$  and wavelength are investigated, respectively. The proposed V-DC-PCF PBS has the good comprehensive performances, including the  $SL$  of 188  $\mu\text{m}$ ,  $IL$  of less than 0.22 dB, and  $SB$  of covering the E + S + C + L + U band. It is believed that the proposed V-DC-PCF PBS can find important applications in the laser, sensing, and dense wavelength division multiplexing systems.

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**Conflicts of Interest:** The authors declare no conflict of interest.

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